Combustion

chamber

**Products** 

15-73 A high efficiency gas furnace burns gaseous propane  $C_3H_8$  with 140 percent theoretical air. The volume flow rate of water condensed from the product gases is to be determined.

Assumptions 1 Combustion is complete. 2 The combustion products contain CO<sub>2</sub>, H<sub>2</sub>O, O<sub>2</sub>, and N<sub>2</sub> only.

Properties The molar masses of C, H<sub>2</sub>, O<sub>2</sub> and air are 12 kg/kmol, 2 kg/kmol, 32 kg/kmol, and 29 kg/kmol, respectively (Table A-1).

Analysis The reaction equation for 40% excess air (140% theoretical air) is

$$C_3H_8 + 1.4a_{th}[O_2 + 3.76N_2] \longrightarrow BCO_2 + DH_2O + EO_2 + FN_2$$

where  $a_{th}$  is the stoichiometric coefficient for air. We have automatically accounted for the 40% excess air by using the factor 1.4 $a_{th}$  instead of  $a_{th}$  for air. The coefficient  $a_{th}$  and other coefficients are to be determined from the mass balances

Carbon balance:

 $2D = 8 \longrightarrow D = 4$ Hydrogen balance: Oxygen balance:  $2 \times 1.4 a_{th} = 2B + D + 2E$ 

 $0.4a_{\rm th} = E$ 

 $1.4a_{th} \times 3.76 = F$ Nitrogen balance:

Solving the above equations, we find the coefficients (E = 2,

F = 26.32, and  $a_{th} = 5$ ) and write the balanced reaction equation as

$$C_3H_8 + 7[O_2 + 3.76N_2] \longrightarrow 3CO_2 + 4H_2O + 2O_2 + 26.32N_2$$

The partial pressure of water in the saturated product mixture at the dew point is

$$P_{v,\text{prod}} = P_{\text{sat@}40^{\circ}\text{C}} = 7.3851 \text{ kPa}$$

The vapor mole fraction is

$$y_v = \frac{P_{v,\text{prod}}}{P_{\text{prod}}} = \frac{7.3851 \,\text{kPa}}{100 \,\text{kPa}} = 0.07385$$

The kmoles of water condensed is determined from

$$y_v = \frac{N_{\text{water}}}{N_{\text{total, product}}} \longrightarrow 0.07385 = \frac{4 - N_{\text{w}}}{3 + 4 - N_{\text{w}} + 2 + 26.32} \longrightarrow N_{\text{w}} = 1.503 \text{ kmol}$$

The steady-flow energy balance is expressed as

$$\dot{N}_{\text{fuel}} H_R = \dot{Q}_{\text{fuel}} + \dot{N}_{\text{fuel}} H_P$$

where 
$$\dot{Q}_{\text{fuel}} = \frac{\dot{Q}_{\text{out}}}{\eta_{\text{furnace}}} = \frac{31,650 \text{ kJ/h}}{0.96} = 32,969 \text{ kJ/h}$$

$$H_R = \overline{h}_f^o_{\text{fuel@25°C}} + 7\overline{h}_{\text{O2@25°C}} + 26.32\overline{h}_{\text{N2@25°C}}$$
  
=  $(-103,847 \text{ kJ/kmol}) + 7(0) + 26.32(0) = -103,847 \text{ kJ/kmol}$ 

$$\begin{split} H_P &= 3\overline{h}_{\text{CO2@25^{\circ}C}} + 4\overline{h}_{\text{H2O@25^{\circ}C}} + 2\overline{h}_{\text{O2@25^{\circ}C}} + 26.32\overline{h}_{\text{N2@25^{\circ}C}} + N_{\text{w}}(\overline{h}_{f \text{ H2O(liq)}}^{o}) \\ &= 3(-393,520 \text{ kJ/kmol}) + 4(-241,820 \text{ kJ/kmol}) + 2(0) + 26.32(0) + 1.503(-285,830 \text{ kJ/kmol}) \\ &= -2.577 \times 10^6 \text{ kJ/kmol} \end{split}$$

Substituting into the energy balance equation,

$$\dot{N}_{\rm fuel} H_R = \dot{Q}_{\rm fuel} + \dot{N}_{\rm fuel} H_P$$

$$\dot{N}_{\rm fuel}$$
 (-103,847 kJ/kmol) = 32,969 kJ/h +  $\dot{N}_{\rm fuel}$  (-2.577×10<sup>6</sup> kJ/kmol)  $\longrightarrow \dot{N}_{\rm fuel}$  = 0.01333 kmol/h

The molar and mass flow rates of the liquid water are

$$\dot{N}_{\rm w} = N_{\rm w} \dot{N}_{\rm fuel} = (1.503 \text{ kmol/kmol fuel})(0.01333 \text{ kmol fuel/h}) = 0.02003 \text{ kmol/h}$$

$$\dot{m}_{\rm w} = \dot{N}_{\rm w} M_{\rm w} = (0.02003 \text{ kmol/h})(18 \text{ kg/kmol}) = 0.3608 \text{ kg/h}$$

The volume flow rate of liquid water is

$$\dot{\mathbf{V}}_{w} = (\mathbf{v}_{f@25^{\circ}C})\dot{m}_{w} = (0.001003 \text{ m}^{3}/\text{kg})(0.3608 \text{ kg/h}) = 0.0003619 \text{ m}^{3}/\text{h} = \mathbf{8.7 L/day}$$