8-79 A rigid tank initially contains saturated R-134a vapor. The tank is connected to a supply line, and R-134a is allowed to enter the tank. The mass of the R-134a that entered the tank and the exergy destroyed during this process are to be determined.

Assumptions 1 This is an unsteady process since the conditions within the device are changing during the process, but it can be analyzed as a uniform-flow process since the state of fluid at the inlet remains constant. 2 Kinetic and potential energies are negligible. 3 There are no work interactions involved. 4 The direction of heat transfer is to the tank (will be verified).

Properties The properties of refrigerant are (Tables A-11 through A-13)

$$P_{1} = 1.2 \text{ MPa}$$

$$\text{sat. vapor} \begin{cases} \mathbf{v}_{1} = \mathbf{v}_{g@1.2 \text{ MPa}} = 0.01672 \text{ m}^{3} / \text{kg} \\ u_{1} = u_{g@1.2 \text{ MPa}} = 253.81 \text{ kJ/kg} \\ s_{1} = s_{g@1.2 \text{ MPa}} = 0.91303 \text{ kJ/kg} \cdot \text{K} \end{cases}$$

$$T_{2} = 1.4 \text{ MPa}$$

$$\text{sat. liquid} \begin{cases} \mathbf{v}_{2} = \mathbf{v}_{f@1.4 \text{ MPa}} = 0.0009166 \text{ m}^{3} / \text{kg} \\ u_{2} = u_{f@1.4 \text{ MPa}} = 125.94 \text{ kJ/kg} \\ s_{2} = s_{f@1.4 \text{ MPa}} = 0.45315 \text{ kJ/kg} \cdot \text{K} \end{cases}$$

$$P_{i} = 1.6 \text{ MPa}$$

$$h_{i} = 93.56 \text{ kJ/kg}$$

$$S_{i} = 0.34554 \text{ kJ/kg} \cdot \text{K}$$

$$R-134a$$

$$0.1 \text{ m}^{3}$$

$$1.2 \text{ MPa}$$

$$Sat. \text{ vapor} \end{cases}$$

Analysis We take the tank as the system, which is a control volume. Noting that the microscopic energies of flowing and nonflowing fluids are represented by enthalpy h and internal energy u, respectively, the mass and energy balances for this uniform-flow system can be expressed as

Mass balance:

$$m_{\rm in} - m_{\rm out} = \Delta m_{\rm system} \rightarrow m_i = m_2 - m_1$$

Energy balance:

$$\begin{array}{ll} E_{\rm in} - E_{\rm out} &= \Delta E_{\rm system} \\ \text{Net energy transfer} \\ \text{by heat, work, and mass} & \text{Change in internal, kinetic,} \\ Q_{\rm in} + m_i h_i &= m_2 u_2 - m_1 u_1 \quad \text{(since } W \cong \text{ke} \cong \text{pe} \cong 0) \end{array}$$

(a) The initial and the final masses in the tank are

$$m_1 = \frac{\mathbf{V}_1}{\mathbf{v}_1} = \frac{0.1 \text{ m}^3}{0.01672 \text{ m}^3/\text{kg}} = 5.983 \text{ kg}$$

 $m_2 = \frac{\mathbf{V}_2}{\mathbf{v}_2} = \frac{0.1 \text{ m}^3}{0.0009166 \text{ m}^3/\text{kg}} = 109.10 \text{ kg}$

Then from the mass balance

$$m_i = m_2 - m_1 = 109.10 - 5.983 = 103.11 \text{ kg}$$

The heat transfer during this process is determined from the energy balance to be

$$Q_{\text{in}} = -m_i h_i + m_2 u_2 - m_1 u_1$$

= -\((103.11 \text{ kg}\)(93.56 \text{ kJ/kg}) + (109.10)\((125.94 \text{ kJ/kg}\)) - \((5.983 \text{ kg})\)(253.81 \text{ kJ/kg}\)
= 2573 \text{ kJ}

(b) The exergy destroyed during a process can be determined from an exergy balance or directly from its definition $X_{\text{destroyed}} = T_0 S_{\text{gen}}$. The entropy generation S_{gen} in this case is determined from an entropy balance on an extended system that includes the tank and its immediate surroundings so that the boundary temperature of the extended system is the surroundings temperature T_{surr} at all times. It gives

$$\frac{S_{\text{in}} - S_{\text{out}}}{S_{\text{entropy transfer}}} + \underbrace{S_{\text{gen}}}_{\text{Entropy generation}} = \underbrace{\Delta S_{\text{system}}}_{\text{Change in entropy}}$$

$$\frac{Q_{\text{in}}}{T_{\text{b,in}}} + m_i s_i + S_{\text{gen}} = \Delta S_{\text{tank}} = (m_2 s_2 - m_1 s_1)_{\text{tank}} \text{ Substituting, the exergy destruction}$$

$$S_{\text{gen}} = m_2 s_2 - m_1 s_1 - m_i s_i - \underbrace{Q_{\text{in}}}_{T_0}$$

is determined to be

$$X_{\text{destroyed}} = T_0 S_{\text{gen}} = T_0 \left[m_2 s_2 - m_1 s_1 - m_i s_i - \frac{Q_{\text{in}}}{T_0} \right]$$

$$= (318 \text{ K}) \left[109.10 \times 0.45315 - 5.983 \times 0.91303 - 103.11 \times 0.34554 - (2573 \text{ kJ}) / (318 \text{ K}) \right]$$

$$= 80.3 \text{ kJ}$$