

9-143 A turbojet aircraft flying at an altitude of 9150 m is operating on the ideal jet propulsion cycle. The velocity of exhaust gases, the propulsive power developed, and the rate of fuel consumption are to be determined.

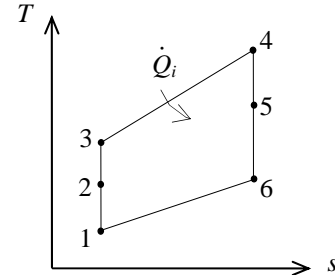
Assumptions 1 Steady operating conditions exist. 2 The air standard assumptions are applicable. 3 Air is an ideal gas with constant specific heats at room temperature. 4 Kinetic and potential energies are negligible, except at the diffuser inlet and the nozzle exit. 5 The turbine work output is equal to the compressor work input.

Properties The properties of air at room temperature are $c_p = 1.005 \text{ kJ/kg} \cdot \text{K}$ and $k = 1.4$ (Table A-2a).

Analysis (a) We assume the aircraft is stationary and the air is moving towards the aircraft at a velocity of $V_1 = 320 \text{ m/s}$. Ideally, the air will leave the diffuser with a negligible velocity ($V_2 \cong 0$).

Diffuser:

$$\begin{aligned}\dot{E}_{\text{in}} - \dot{E}_{\text{out}} &= \Delta \dot{E}_{\text{system}}^{\phi_0 \text{ (steady)}} \longrightarrow \dot{E}_{\text{in}} = \dot{E}_{\text{out}} \\ h_1 + V_1^2 / 2 &= h_2 + V_2^2 / 2 \longrightarrow 0 = h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} \\ 0 &= c_p (T_2 - T_1) - V_1^2 / 2 \\ T_2 &= T_1 + \frac{V_1^2}{2c_p} = 241 \text{ K} + \frac{(320 \text{ m/s})^2}{(2)(1.005 \text{ kJ/kg} \cdot \text{K}) \left(\frac{1 \text{ kJ/kg}}{1000 \text{ m}^2/\text{s}^2} \right)} = 291.9 \text{ K} \\ P_2 &= P_1 \left(\frac{T_2}{T_1} \right)^{k/(k-1)} = (32 \text{ kPa}) \left(\frac{291.9 \text{ K}}{241 \text{ K}} \right)^{1.4/0.4} = 62.6 \text{ kPa}\end{aligned}$$



Compressor:

$$\begin{aligned}P_3 &= P_4 = (r_p)(P_2) = (12)(62.6 \text{ kPa}) = 751.2 \text{ kPa} \\ T_3 &= T_2 \left(\frac{P_3}{P_2} \right)^{(k-1)/k} = (291.9 \text{ K})(12)^{0.4/1.4} = 593.7 \text{ K}\end{aligned}$$

Turbine:

$$w_{\text{comp,in}} = w_{\text{turb,out}} \longrightarrow h_3 - h_2 = h_4 - h_5 \longrightarrow c_p (T_3 - T_2) = c_p (T_4 - T_5)$$

or $T_5 = T_4 - T_3 + T_2 = 1400 - 593.7 + 291.9 = 1098.2 \text{ K}$

Nozzle:

$$\begin{aligned}T_6 &= T_4 \left(\frac{P_6}{P_4} \right)^{(k-1)/k} = (1400 \text{ K}) \left(\frac{32 \text{ kPa}}{751.2 \text{ kPa}} \right)^{0.4/1.4} = 568.2 \text{ K} \\ \dot{E}_{\text{in}} - \dot{E}_{\text{out}} &= \Delta \dot{E}_{\text{system}}^{\phi_0 \text{ (steady)}} \longrightarrow \dot{E}_{\text{in}} = \dot{E}_{\text{out}} \\ h_5 + V_5^2 / 2 &= h_6 + V_6^2 / 2 \\ 0 &= h_6 - h_5 + \frac{V_6^2 - V_5^2}{2} \longrightarrow 0 = c_p (T_6 - T_5) + V_6^2 / 2 \\ \text{or } V_6 &= \sqrt{(2)(1.005 \text{ kJ/kg} \cdot \text{K})(1098.2 - 568.2) \text{ K} \left(\frac{1000 \text{ m}^2/\text{s}^2}{1 \text{ kJ/kg}} \right)} = 1032 \text{ m/s}\end{aligned}$$

(b) $\dot{W}_p = \dot{m}(V_{\text{exit}} - V_{\text{inlet}})V_{\text{aircraft}} = (60 \text{ kg/s})(1032 - 320) \text{ m/s}(320 \text{ m/s}) \left(\frac{1 \text{ kJ/kg}}{1000 \text{ m}^2/\text{s}^2} \right) = 13,670 \text{ kW}$

(c) $\dot{Q}_{\text{in}} = \dot{m}(h_4 - h_3) = \dot{m}c_p (T_4 - T_3) = (60 \text{ kg/s})(1.005 \text{ kJ/kg} \cdot \text{K})(1400 - 593.7) \text{ K} = 48,620 \text{ kJ/s}$

$$\dot{m}_{\text{fuel}} = \frac{\dot{Q}_{\text{in}}}{\text{HV}} = \frac{48,620 \text{ kJ/s}}{42,700 \text{ kJ/kg}} = 1.14 \text{ kg/s}$$